

TE 364: Communication Circuits Lecture 4

Radio Receivers & Characterization

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Outline



Radio Recivers

- Superheterodyne Receivers
 Analog
 Digital
 Receiver Characterization
 - Receiver Noise
 - Receiver Sensitivity
 - System Non-linearity
 - Receiver Dynamic Range

Receiver Selectivity



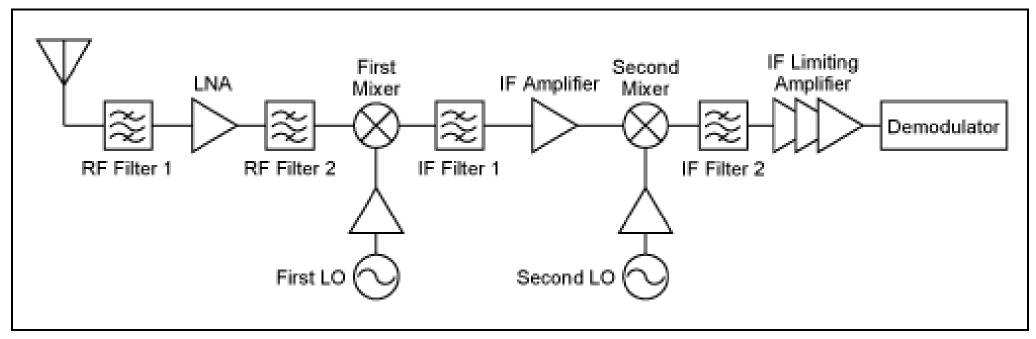


Fig. 1 The Superheterodyne receiver



KNUST Telecomm.

Engineering



The antenna: functions as described earlier

RF Preselector

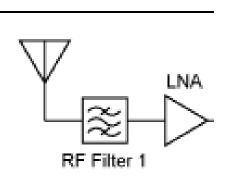
*Filter out all unwanted frequencies outside RF band

Eliminate spurious response

RF Amplifier

\$ linearly amplify input signal & minimize added noise

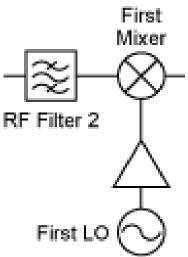
Low noise amplifiers are typically used for this purpose







- The Interstage selector
 - suppresses gain of any undesired signal responses at spurious frequencies
 - >and at image frequencies in particular
 - Thus maintaining system noise figure
- The Local Oscillator (LO)
 - Tuned across a bandwidth equal to the RF bandwidth
 - Generates strong carrier signal for mixing with mixer







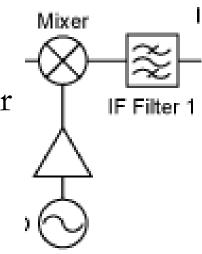
The First Mixer

translates signals @ RF to IF frequency signal
Depending on the frequency of the LO
Phase information of signal preserved by the mixer
Due to linear translation of frequency
IF frequencies from 45 to 82 MHz are common
for mobile radio receivers in the 800 MHz band.

The IF Filter

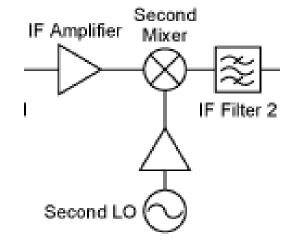
Rejects spurious signals generated by the mixer







- The IF amplifier
 - provides adequate gain to the IF signal
 - ➤To drive the next stage
 - ≻Can provide high gain and is well-stabilized
 - ✤IF frequencies from 45 to 82 MHz are common
 - > for mobile radio receivers in the 800 MHz band.
- The Second mixer, LO and second IF Filter
 - Mirror the function of the first IF strip
 - Narrows in and select the desired channel fro the entire passband

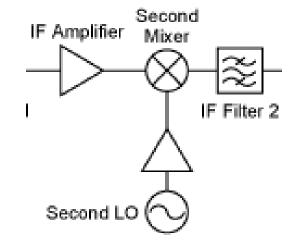






- The Second mixer, LO and second IF Filter
 - Provides additional selectivity for the receiver
 - *455 kHz is a fairly standard second IF frequency
 - Mobile phone receivers' IF frequency
 - ≻Typically 10 MHz
- In some architectures,
 - second IF stage is omitted.
 - Single down-conversion to a low IF
 - ✤IF filter then performs channel selection







The Demodulator

Extracts modulated signal from IF signal

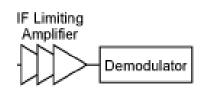
Converts the modulated signal to baseband

- ≻AM or FM (Analog system)
- Multi-amplitude symbols or multiphase levels symbol

• Decoded to recover original signal.

The Baseband amplifier

provides output power to drive output device
 Typicall speaker, fax or video screen



The Super Heterodyne Receiver-Digital System



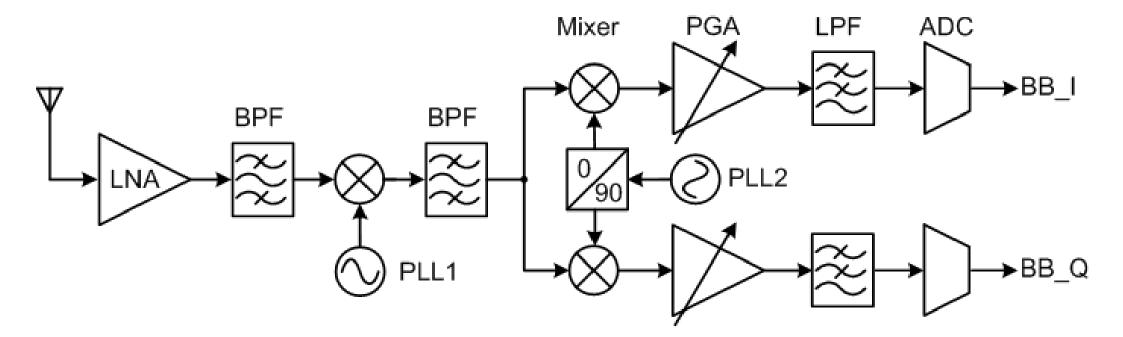


Fig. 2 The Superheterodyne receiver



The Super Heterodyne Receiver-Digital System



- Two parallel output stages
 - ✤In-phase (I signal)
 - Quadrature-Phase (Q signal)
- Allows both amplitude and phase information to be preserved.
- Requires two mixers
 - **One** $driven by an LO signal of the form <math>\cos \omega_{LO} t$
 - *****The other $\sin \omega_{LO} t$
- $\Box I$ and Q channels \Rightarrow 1 and 0 of binary signal.



A/D converter



•For flat top sampling

- *a sample-and-hold circuit is used
- together with the chopper
- This holds the amplitude of each pulse at constant level during sampling time
 MESSAGE SAMPLE

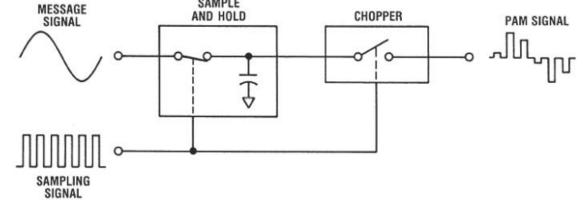
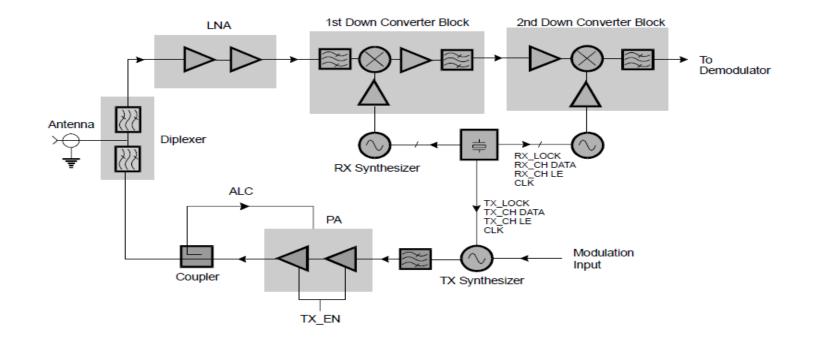


Fig. 3: Flat-top Sampling



Analog Transceiver System





A block diagram of an analog mobile phone handsets



The Communication Channel



Hartley-Shannon Theorem

Relates Channel Capacity to
Channel Bandwidth, *B* and
Signal-to-Noise Ratio, *S/N*

$$C = B \log_2\left(1 + \frac{S}{N}\right) \text{ bits/sec}$$

✤It is a trade-off relation

Setween bandwidth and S/N ratio

►GSM vs CDMA



Receiver Noise



Sources of Noise

- *The channel, through to the antenna
- The RF preselector filter:
 - ➢Thermal noise contribution
- The active devices:
 - ≻Thermal noise
 - ≻Shot noise
 - >Flicker noise (1/f noise)



Receiver Noise...



Thermal Noise Power

$$P_N = kTB$$

- ✤k is Boltzmann's constant,
- T is temperature,

A is the bandwidth over which measurement is made.

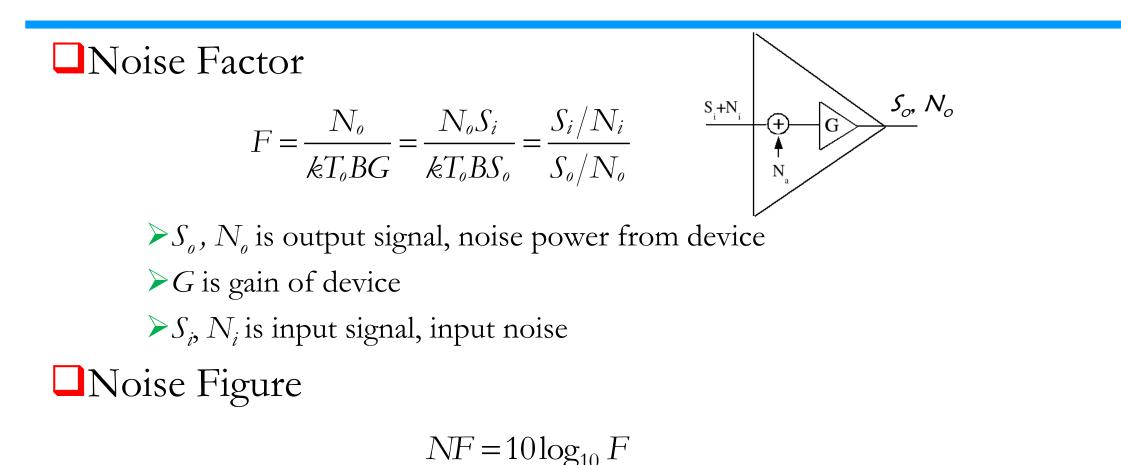
$$P_N = (1.38 \times 10^{-23} J / K) (293K) (1Hz)$$

= 4.057 × 10⁻²¹ W
=-174 dBm



Receiver Noise...



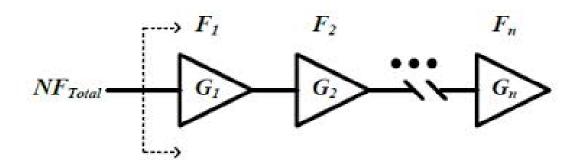




Receiver Noise...



□Noise Factor of cascaded system



Total Noise Factor

$$F_{tot} = F_1 + (F_2 - 1)/G_1 + (F_3 - 1)/G_1 G_2 + \cdots + (F_n - 1)/G_1 G_2 \cdots G_{n-1}$$



Receiver Sensitivity



□Noise floor of the receiver prior to detection determines

- How strong the input signal must to be correctly interpreted as
 - >0 or 1 in a digital system or
 - ≻High-quality analog waveform in analog system
- **Receiver** Sensitivity is
 - Minimum input signal strength to produce quality output signal in the receiver.



Receiver Sensitivity



- □Noise floor of the receiver referred to the
 - input, called
 - Minimum detectable signal is used as measure of
 - sensitivity
 - ◆Signal to noise ratio of 10 dB considered minimum for audiofiles
 >S₀/N₀ of 10 dB is used to measure sensitivity
 >Or a SINAD (Signal in Noise and Distortion) of 10 dB
 ◆BER (Bit Error Rate) is another measure of sensiti-vity in digital
 - systems: BER of 1% specified





A component is nonlinear when

- Its output amplitude is not linearly proportional to its input amplitude or
- Its output phase is not linearly proportional to its input phase.
- Gross nonlinearity
 - Results from cut-off and saturation effects
 - >Occurs as device exceeds the limits of its normal active region
 - *gain compression, intermodulation distortion





In most active devices,

- *nonlinearity is due to
 - Amplitude induced change in device transconductance
- Collector or drain current modelled as a nonlinear

function of the input voltage, v_{in} .

$$I_{o} = I_{Q} + g_{m}v_{IN} + g_{m2}v_{IN}^{2} + g_{m3}v_{IN}^{3} + \cdots$$

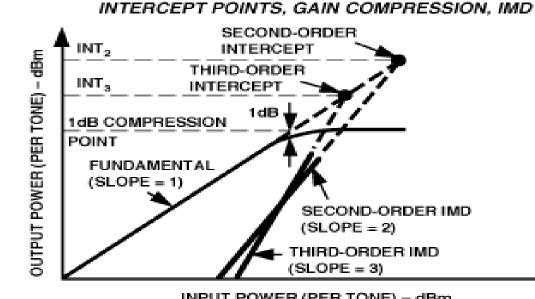
leads to 3rd order intermodulation products

Harmonic powers increase nonlinearly with input





Third-order distortion and gain compression



Other measure of nonlinearity includes

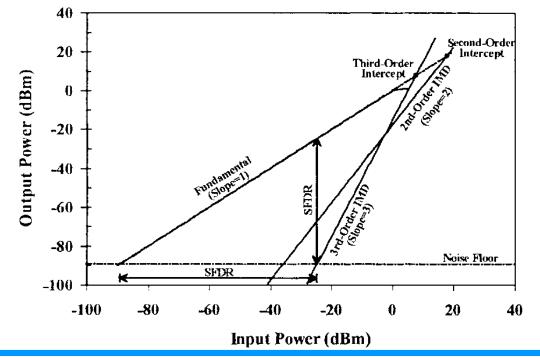
Adjacent Channel Power Ratio (ACPR)





Receiver Dynamic Range

Difference between the minimum detectable signal and the maximum signal



SFDR is Spurious-free dynamic range

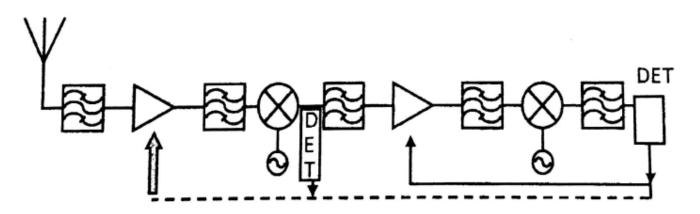


- Automatic Gain Control (AGC)
 - ♦ Gain of a system automatically controlled such that:
 - >Decrease gain when strong signal cause overload
 - or distortion
 - Thus increasing the useful range of a receiver
- Trade of is sometimes required
 - Example: AGC verses noise performance of LNA
 - Attenuation in front of LNA
 - ≻Reduces gain but
 - ➢Worsens noise figure of LNA





Automatic Gain Control (AGC)



Gain reduced to minimize distortion

Output stage gain ideally reduced first

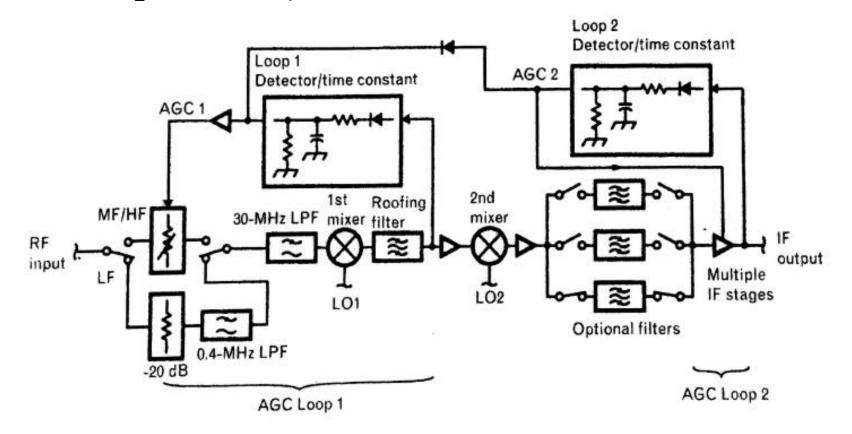
>This prevents noise figure of system rising

*AGC is then introduced progressively ahead of them





Dual Loop AGC System







Selectivity

- Refers to the ability of a filter to reject signal outside its pass-band.
- Defined by the attenuation of a signal at some frequencies offset from its center frequency.
- *For channel selection filters in radio receivers,
 - Selectivities of 60 dB to 80 dB are typical
- Selectivity of radio receiver measured in terms of
 - Relative strength of adjacent signal compared to desired signal.
 Eg. 60 dBc to 80 dBc.





Spurious responses

Outputs that arise from unwanted frequency

components

Demodulating a channel whose carrier is at 895 MHz

➤A signal at 890 MHz can create a response in the receiver that interferes wit h the channel at 895 MHz.

The 890 MHz signal is thus a spurious signal

Spurious response can reduce the selectivity of a receiver.





Spurious responses

- Although the amplitudes of spurious signals cannot be quantitatively determined, their frequencies can be known.
- Looking at the mixer as a source of spurious responses
 - $> f_{\rm T}$ is desired signal frequency to which receiver is tuned
 - $> f_s$ is unwanted spurious frequency
 - ► In the mixer, sum and difference frequencies will produce with the mixer's L O frequency, f_{o}





Spurious responses

- *****For sum mixer: $f_o + f_T = f_{IF}$
- For difference mixer (high side LO): $f_o f_T = f_{IF}$
- ***** For difference mixer (Low side LO): $f_o f_T = -f_{IF}$

At multiple harmonics, spurious response could also map to IF
◆For sum mixer: nf_o + mf_s = f_{IF}
◆For difference mixer (high side LO): nf_o - mf_s = f_{IF}
◆For difference mixer (Low side LO): nf_o - mf_s = -f_{IF}





 \Box Normalizing by f_{IF} and defining

$$T = f_T / f_{IF}$$
$$O = f_o / f_{IF}$$
$$S = f_s / f_{IF}$$

Eliminating O from both sets of equations

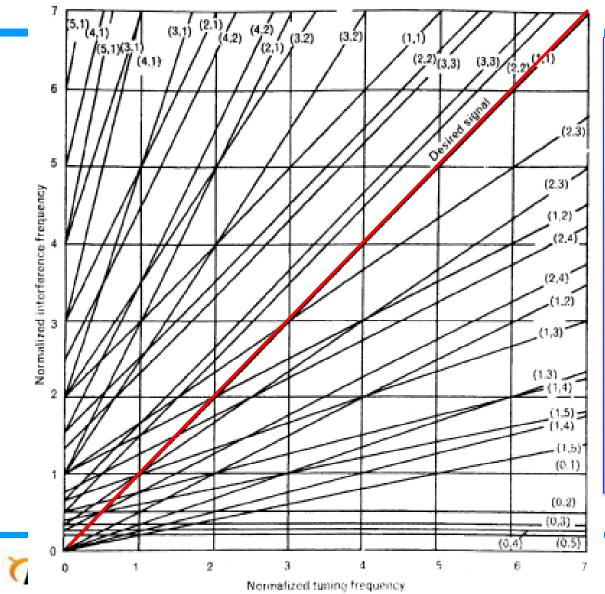
- ***** For sum mixer: n(1-T) + mS = 1
- For difference mixer (high side LO): $n(T+1) mS = \pm 1$

For difference mixer (Low side LO): $n(T-1) - mS = \pm 1$



Spurious response Chart





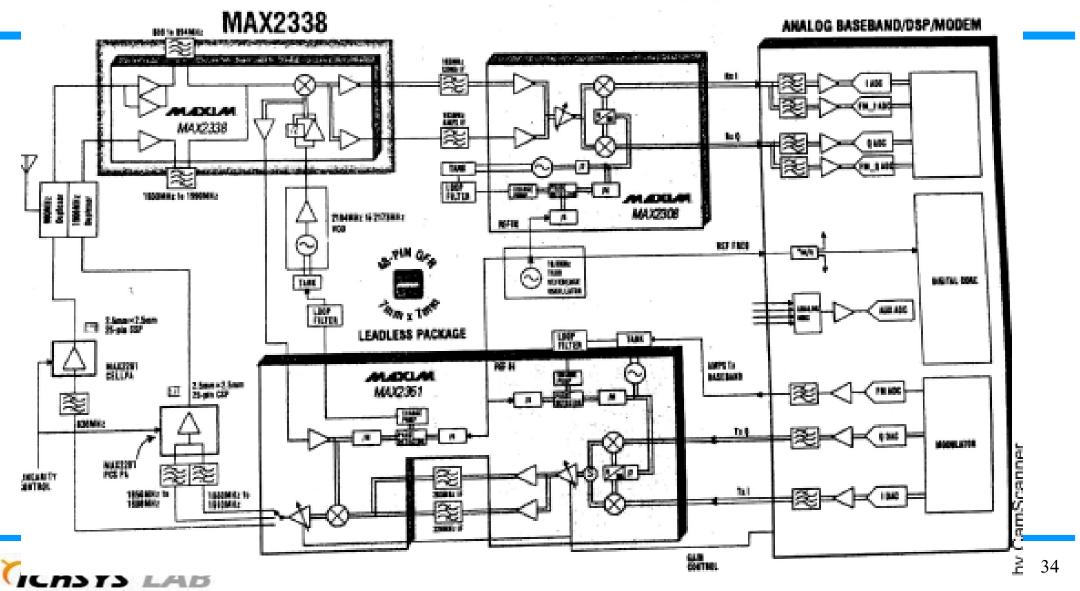
Difference Mixer

If f_{IF} is 45 MHz And f_T is 135 MHz Then f_O is 180 MHz T=135/45=3

Spurious response will be caused by a spurious signal at the same frequency as the tuned signal S=3 generated by (2,3) mixing produ cts Consider f_T between 90 and 180 MHz

CDMA Receiver Handset





Air-Interface specification for PCS CDMA Mobile Handset



TABLE 3.1 SOME PARAMETERS FROM THE IS-95/98 AIR-INTERFACE SPECIFICATIONS FOR THE PCS CDMA Mobile Handset

MEASUREMENT PARAMETER	SPECIFICATION
Receive frequency band	1,930–1,990 MHz
Transmit frequency band	1,850–1,910 MHz
Peak frequency deviation (channel bandwidth)	1,230 kHz
Maximum input power (total power at antenna connector) for error rate < 1/2%	-25 dBm
Minimum detectable signal (total power at antenna connector) for error rate < 1/2%	-104 dBm
Detection in presence of low level interference (error rate < 1%)	Detect a tone at -101 dBm in the presence of two interfering tones at -43 dBm each, offset 900 kHz and 1,700 kHz from cen- ter of channel
Transmitter output power	+23 dBm to -50 dBm
Maximum adjacent channel strength at 885-kHz offset	-42 dBc integrated over a 30-kHz bandwidth
Maximum alternate channel strength at 1,980-kHz offset	-54 dBc integrated over a 30-kHz bandwidth

CDMA Receiver Handset



Core components in the receiver chain

